# Parametrization of ternary nucleation rates for H<sub>2</sub>SO<sub>4</sub>-NH<sub>3</sub>-H<sub>2</sub>O vapors

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[1] A parametrization of nucleation rates for  $H_2O-H_2SO_4-NH_3$  vapors in atmospheric conditions is developed. The parametrization is based on nucleation rates obtained from a self-consistent model of ternary nucleation, including state-of-art thermodynamics, H<sub>2</sub>O-H<sub>2</sub>SO<sub>4</sub> hydration model, and rigorous treatment of nucleation kinetics. The parametrized nucleation rates are shown to be within one order of magnitude from those given by the full model with enhanced accuracy at higher nucleation rates. Parametrizations for particle numbers and radius of the critical nucleus are given as a function of nucleation rate and temperature. The parametrizations are valid for temperatures 240-300 K, relative humidities 5-95%, sulfuric acid concentrations  $10^4 - 10^9$  molecules cm<sup>-3</sup>, ammonia mixing ratios 0.1–100 ppt, and nucleation rates  $10^{-5} - 10^{6} \text{ cm}^{-3} \text{ s}^{-1}$ . INDEX TERMS: 0305 Atmospheric Composition and Structure: Aerosols and particles (0345, 4801); 0365 Atmospheric Composition and Structure: Troposphere-composition and chemistry; 0322 Atmospheric Composition and Structure: Constituent sources and sinks; KEYWORDS: water, sulfuric acid, ammonia, nucleation

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#### Introduction 1.

[2] Experimental and theoretical progress in recent years has shown the importance of homogeneous nucleation in new particle production in the atmosphere [Weber et al., 1999; Kulmala et al., 2000]. In addition to water vapor, the nucleation process typically involves one or more trace compounds which may have crucial role in the formation of stable aerosol particles. In this respect the most studied example is the conucleation of water and sulfuric acid [e.g., Kulmala et al., 1998; Seinfeld and Pandis, 1998]. However, in many cases the observed atmospheric particle formation rates greatly exceed those expected on the basis of binary H<sub>2</sub>O-H<sub>2</sub>SO<sub>4</sub> nucleation alone, for example, in marine [Covert et al., 1992; Hoppel et al., 1994] and coastal [O'Dowd et al., 1999] boundary layer and in boreal forests [Mäkelä et al., 1997; Kulmala et al., 2001]. Although several explanations have been proposed to explain the enhanced particle production (e.g., ioninduced nucleation [Turco et al., 1998]), the most obvious explanation is the participation of a third chemical component in the nucleation process [Kulmala et al., 2000]. The most likely candidate is ammonia because of its abundance in the atmosphere and its ability to lower the vapor pressure H<sub>2</sub>SO<sub>4</sub> above the solution, which is expected to enhance particle formation in gases containing

H<sub>2</sub>SO<sub>4</sub> [Scott and Cattell, 1979; Coffmann and Hegg, 1995].

[3] In ternary nucleation rather complex thermodynamics and chemistry of H<sub>2</sub>O-H<sub>2</sub>SO<sub>4</sub>-NH<sub>3</sub> system are needed [Napari et al., 2002]. In the liquid phase, H<sub>2</sub>SO<sub>4</sub> and NH<sub>3</sub> undergo multiple dissociation and association steps producing various salts and ions. The gas phase behavior is characterized by the formation of water-sulfuric acid hydrates in which one H<sub>2</sub>SO<sub>4</sub> and one or more H<sub>2</sub>O molecules gather into small clusters. Considering these facts, an accurate and comprehensive thermodynamic model is critical to understanding nucleation phenomena in H<sub>2</sub>O-H<sub>2</sub>SO<sub>4</sub>-NH<sub>3</sub> vapors. Due to the complex thermodynamics and detailed nucleation kinetics [Napari et al., 2002] the calculation of nucleation rate is computationally very demanding. In order to be able to use ternary nucleation scheme as a part of aerosol dynamic models or even in 3-D atmospheric models parametrizations are urgently needed.

[4] The purpose of this paper is to present an up-to-date parametrized equation for nucleation rates in H<sub>2</sub>O-H<sub>2</sub>SO<sub>4</sub>-NH<sub>3</sub> vapors. Only those values which are obtained from a recently developed ternary nucleation model [Napari et al., 2002] are used in the fitting procedure. We try to include as wide range of atmospherically relevant parameter values as possible while aiming for accuracy of one order of magnitude at significant nucleation rates.

[5] We first present the ternary nucleation model in a concise form in section 2. The parametrizations are derived in section 3. The full model and the parametrizations are compared in section 4. Finally, discussion and conclusions are presented in section 5.

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## 2. Ternary Nucleation Model

[6] The formation energy  $\Delta G$  of a cluster in a ternary vapor can be written as [*Laaksonen et al.*, 1999]

$$\Delta G = -kT \sum_{i=1}^{3} n_i \ln\left(\frac{p_i}{p_{s,i}}\right) + 4\pi \sigma r^2, \qquad (1)$$

where  $n_i$  are the total number of molecules of each species in the cluster,  $p_i$  is the ambient partial pressure of free molecules of species *i*,  $p_{s,i}$  is the equilibrium vapor pressure of species *i* above a flat surface of a solution with the composition of the nucleus, *r* is the radius of the droplet, *k* is Boltzmann constant, and *T* is temperature. The surface tension of a flat liquid-vapor interface  $\sigma$  is evaluated at the composition of the nucleus. In the present case indices 1, 2, and 3 refer to water, sulfuric acid, and ammonia.

[7] Minimization of equation (1) with respect of particle numbers  $n_i$  results in a pair of equations [*Wilemski*, 1984]

$$\ln\left(\frac{p_1}{p_{s,1}}\right)v_2 = \ln\left(\frac{p_2}{p_{s,2}}\right)v_1,\tag{2}$$

$$\ln\left(\frac{p_3}{p_{s,3}}\right)v_2 = \ln\left(\frac{p_2}{p_{s,2}}\right)v_3,\tag{3}$$

where  $v_i$  is the partial molar volume of species *i*. The composition of the critical nucleus is numerically solved from equations (2) and (3), and the corresponding formation energy is then found from [*Laaksonen et al.*, 1999]

$$\Delta G^* = \frac{4}{3} \pi r^{*2} \sigma, \tag{4}$$

where  $r^*$  is the radius of the critical nucleus.

[8] Once the composition is known, the nucleation rate is obtained from [*Trinkaus*, 1983]

$$J = \frac{|\lambda|/\pi}{\sqrt{-\det(\mathbf{D})/\pi}}\rho(\{n_i\}),\tag{5}$$

where **D** is a matrix with elements

$$D_{ij} = \frac{1}{2kT} \frac{\partial^2 \Delta G(\{n_i\})}{\partial n_i \partial n_j} |_{\{n_i^*\}} \quad (i, j = 1, 2, 3), \tag{6}$$

and  $\lambda$  is the negative eigenvalue of matrix **KD**, where **K** is the condensation matrix [*Binder and Stauffer*, 1976]. The elements of the condensation matrix are related to the collision rate of the vapor particles with the cluster. In our case the colliding particles are water monomers, free acid molecules, free ammonia molecules, or water-acid hydrates containing one acid molecule and up to five water molecules. The equilibrium distribution of clusters containing  $n_i$ molecules of each species  $\rho(\{n_i\})$  is obtained from the selfconsistent equilibrium distribution [*Noppel*, 2000, equation (3)]. The formation energy  $\Delta G$  is obtained from equation (1) and the matrix elements in equation (6) are evaluated at the composition of the critical nucleus with particle numbers  $n_i^*$ .

[9] In the most rigorous form of equation (6) the derivatives are calculated with respect to total number of particles  $n_i = n_{il} + n_{is}$ , where  $n_{il}$  are the numbers of molecules in the uniform liquid phase encompassed by the surface of tension and  $n_{is}$  are the surface excess number of molecules caused by the difference between the density profiles of the uniform Gibbsian droplet model and the actual droplet. However, because of numerical efficiency and stability, we approximate  $n_i \approx n_{il}$  [Napari et al., 2002]; that is, we assume that derivatives do not depend on the surface excess number of particles. The resulting errors in nucleation rates are less than half an order of magnitude.

[10] The calculation of the partial pressures of  $H_2O$  and NH<sub>3</sub> is based on the thermodynamic model of *Clegg et al.* [1998] (available as http://www.hpc1.uea.ac.uk/~e770/ aim.html). The partial pressure of  $H_2SO_4$  is estimated as described by *Noppel et al.* [2002]. Details of the hydration model are given by *Napari et al.* [2002] and *Noppel et al.* [2002]. Surface tension and density of the solution are approximated using the method of *Van Dingenen and Raes* [1993]; however, instead of direct application of this method to  $H_2O-H_2SO_4-NH_3$  system, surface tension and density are also fitted to binary limits of (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>-H<sub>2</sub>O and NH<sub>4</sub>HSO<sub>4</sub>-H<sub>2</sub>O [*Korhonen et al.*, 1999].

#### 3. Parametrization of Nucleation Rate Values

[11] In this section we present a parametrization of ternary nucleation rates  $J(T, RH, c, \xi)$ , where *T* is temperature, *RH* is relative humidity, *c* is H<sub>2</sub>SO<sub>4</sub> concentration, and  $\xi$  is NH<sub>3</sub> mixing ratio. In addition, we give the number of different types of molecules in the critical nuclei and the radius of the nuclei as a function of nucleation rate and temperature. The parametrizations are based on data generated using the full nucleation model outlined in the previous section.

[12] In order to construct the parametrization for nucleation rate we first searched for functional dependencies by keeping three variables constant at a time. We soon found that a polynomial fit reproduced the nucleation rates at a constant temperature quite accurately if polynomials of *RH*, ln *RH*, ln *c*, 1/ln *c*, and ln  $\xi$  were used in the fitting. However, the temperature dependence was harder to fit according to this scheme, because at high temperatures nucleation rate is a very strong function of temperature whereas at low temperatures the temperature dependence is virtually nonexistent [*Napari et al.*, 2002]. Notwithstanding, we were able to account for the temperature dependence of the coefficients in the aforementioned polynomial expansion by fitting each of the coefficients to a third-order polynomial of temperature.

[13] The resulting fit has the form

$$\ln J_{\text{fit}} = -84.7551 + \frac{f_1(T)}{\ln c} + f_2(T) \ln c + f_3(T) \ln^2 c + f_4(T) \ln \xi + f_5(T) \ln^2 \xi + f_6(T)RH + f_7(T) \ln RH + f_8(T) \frac{\ln \xi}{\ln c} + f_9(T) \ln \xi \ln c + f_{10}(T)RH \ln c + f_{11}(T) \frac{RH}{\ln c} + f_{12}(T)RH \ln \xi + f_{13}(T) \frac{\ln RH}{\ln c} + f_{14}(T) \ln RH \ln \xi + f_{15}(T) \frac{\ln^2 \xi}{\ln c} + f_{16}(T) \ln c \ln^2 \xi + f_{17}(T) \ln^2 c \ln \xi + f_{18}(T)RH \ln^2 \xi + f_{19}(T) \frac{RH \ln \xi}{\ln c} + f_{20}(T) \ln^2 c \ln^2 \xi, \quad (7)$$

**6** - 3

$a_{i0}$	$a_{i1}$	$a_{i2}$	$a_{i3}$
-0.355297	-33.8449	0.34536	-0.000824007
3.13735	-0.772861	0.00561204	-9.74576E-6
19.0359	-0.170957	0.000479808	-4.14699E-7
1.07605	1.48932	-0.00796052	7.61229E-6
6.0916	-1.25378	0.00939836	-0.0000174927
0.31176	1.64009	-0.00343852	-0.0000109753
-0.0200738	-0.752115	0.00525813	-8.98038E-6
0.165536	3.26623	-0.0489703	0.000146967
6.52645	-0.258002	0.00143456	-2.02036E-6
3.68024	-0.204098	0.00106259	-1.2656E-6
-0.066514	-7.82382	0.0122938	0.0000618554
0.65874	0.190542	-0.00165718	3.41744E-6
0.0599321	5.96475	-0.0362432	0.0000493337
-0.732731	-0.0184179	0.000147186	-2.37711E-7
0.728429	3.64736	-0.027422	0.0000493478
41.3016	-0.35752	0.000904383	-5.73788E-7
-0.160336	0.00889881	-0.0000539514	8.39522E-8
8.57868	-0.112358	0.000472626	-6.48365E-7
0.0530167	-1.98815	0.0157827	-0.0000293564
-2.32736	0.0234646	-0.000076519	8.0459E-8
	$\begin{array}{c} a_{i0} \\ \hline \\ -0.355297 \\ 3.13735 \\ 19.0359 \\ 1.07605 \\ 6.0916 \\ 0.31176 \\ -0.0200738 \\ 0.165536 \\ 6.52645 \\ 3.68024 \\ -0.066514 \\ 0.65874 \\ 0.0599321 \\ -0.732731 \\ 0.728429 \\ 41.3016 \\ -0.160336 \\ 8.57868 \\ 0.0530167 \\ -2.32736 \end{array}$	$\begin{array}{c cccc} a_{i0} & a_{i1} \\ \hline & -0.355297 & -33.8449 \\ 3.13735 & -0.772861 \\ 19.0359 & -0.170957 \\ 1.07605 & 1.48932 \\ 6.0916 & -1.25378 \\ 0.31176 & 1.64009 \\ -0.0200738 & -0.752115 \\ 0.165536 & 3.26623 \\ 6.52645 & -0.258002 \\ 3.68024 & -0.204098 \\ -0.066514 & -7.82382 \\ 0.65874 & 0.190542 \\ 0.0599321 & 5.96475 \\ -0.732731 & -0.0184179 \\ 0.728429 & 3.64736 \\ 41.3016 & -0.35752 \\ -0.160336 & 0.00889881 \\ 8.57868 & -0.112358 \\ 0.0530167 & -1.98815 \\ -2.32736 & 0.0234646 \\ \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

**Table 1.** Coefficients of Polynomials  $f_i(T)$ 

Read E-x as  $10^{-x}$ .

where each of the functions  $f_i(T)$  is a third-order polynomial

$$f_i(T) = a_{i0} + a_{i1}T + a_{i2}T^2 + a_{i3}T^3.$$
(8)

The coefficients  $a_{ij}$  are listed in Table 1. Temperature is given in kelvins, H<sub>2</sub>SO<sub>4</sub> concentration in cm<sup>-3</sup>, NH<sub>3</sub> mixing ratio in ppt, and relative humidity as a fraction (e.g., 0.5 corresponding to 50%). Nucleation rate is then obtained in cm<sup>-3</sup> s<sup>-1</sup>.

[14] The limits of validity of the parametrization are T = 240-300 K, RH = 0.05-0.95,  $c = 10^4-10^9$  cm<sup>-3</sup>,  $\xi = 0.1-100$  ppt, and  $J = 10^{-5}-10^6$  cm<sup>-3</sup> s<sup>-1</sup>. The upper limit of nucleation rate is particularly stringent due to the polynomial fit; the parametrized curve as a function of temperature may show an erroneous minimum at low temperatures if nucleation rate exceeds the limit of validity. Also, because of the logarithmic dependencies on RH and c, the parametrization cannot be used to obtain binary H<sub>2</sub>O-H<sub>2</sub>SO<sub>4</sub> or H<sub>2</sub>O-NH<sub>3</sub> limit.

[15] Approximations for the number of particles of each molecular species in the critical nucleus  $n_i^*$  and the radius the cluster  $r^*$  can easily be obtained as functions of nucleation rate and temperature:

$$n_{\rm H_2SO_4}^* = 38.1645 + 0.774106 \ln J + 0.00298879 \ln^2 J -0.357605T - 0.00366358T \ln J + 0.0008553T^2, \quad (9)$$

$$n_{\rm NH_3}^* = 26.8982 + 0.682905 \ln J + 0.00357521 \ln^2 J -0.265748T - 0.00341895T \ln J + 0.000673454T^2,$$
(10)

$$n_{\text{tot}}^* = 79.3484 + 1.7384 \ln J + 0.00711403 \ln^2 J -0.744993T - 0.00820608T \ln J + 0.0017855T^2, (11)$$

$$r^* = 0.141027 - 0.00122625 \ln J - 7.82211 \times 10^{-6} \ln^2 J$$
  
-0.00156727T - 0.00003076T lnJ + 0.0000108375T^2. (12)

where  $n_{\text{H}_2\text{SO}_4}^*$ ,  $n_{\text{NH}_3}^*$ , and  $n_{\text{tot}}^*$  are the numbers (including the surface excess numbers) of H<sub>2</sub>SO<sub>4</sub>, NH<sub>3</sub>, and the total number of particles, respectively. Nucleation rate is given in

cm<sup>-3</sup> s<sup>-1</sup> and temperature in kelvins. The critical radius is obtained in nanometers. As above, validity of the parametrizations is limited to nucleation rates  $J = 10^{-5}-10^6$  cm<sup>-3</sup> s<sup>-1</sup> and temperatures T = 240-300 K. The number water of molecules cannot be fitted according to this simple scheme; however, the water content of the critical clusters in the nucleation rate range considered here is usually less than 0.5 molecules at low temperatures, and can thus be set to zero. At temperatures higher than about 280 K a reasonable estimate of the water content is obtained by subtracting the fitted  $n_{\rm H_2SO_4}^*$  and  $n_{\rm NH_3}^*$  from  $n_{\rm tot}^*$ .

#### 4. Results

[16] The ratio of the fitted nucleation rate (7) and the nucleation rate from the full ternary nucleation model are shown in Figure 1. The parameter values vary over their full range of validity. For nucleation rates higher than  $10^{-3}$  cm<sup>-3</sup> s<sup>-1</sup>, 75% of the ratios  $J_{fit}/J$  are in the range 0.53-1.47 and 95% in the range 0.26-1.74. For  $J = 10^{-6}-10^{-4}$  cm<sup>-3</sup> s<sup>-1</sup> the deviation is somewhat larger, but at such low nucleation rates the reduced accuracy is of lesser consequence. For the whole range of nucleation rates and parameter values we can safely assume that the parametrization is correct to one order of magnitude almost everywhere.

[17] Comparisons of the parametrization for the nucleation rate and the full model calculations at temperatures 258.15 K and 298.15 K are shown in Figures 2–4. In each figure the results from equation (7) are indicated as dotted lines. Figure 2 illustrates the dependence of nucleation rate on total  $H_2SO_4$  concentration (free  $H_2SO_4$  molecules and  $H_2SO_4$  in hydrates) for a pair of NH<sub>3</sub> mixing ratios for both the temperatures. The overall goodness of the fit can be considered as excellent. A similar plot is shown in Figure 3 depicting the dependence of nucleation rate on NH<sub>3</sub> mixing ratio. The largest deviation here is just over one order of



**Figure 1.** Ratio of the fitted nucleation rate  $J_{\text{fit}}$  and the theoretical nucleation rate J. The parameter ranges are T = 240-300 K, RH = 0.05-0.95,  $c = 10^4-10^9$  molecules cm<sup>-3</sup>,  $\xi = 0.1-100$  ppt.



**Figure 2.** Nucleation rate as a function of total  $H_2SO_4$  concentration at T = 258.15 K and T = 298.15 K. Ammonia mixing ratio (in ppt) is indicated for each curve. Nucleation rates obtained from the parametrization are depicted as a dotted line. Relative humidity is 50%.

magnitude. Nucleation rate as a function of relative humidity is shown in Figure 4. The poorest fit is found for the curve with T = 298.15 K and  $\xi = 10$  ppt. Fortunately, the largest discrepancy (about one order of magnitude) occurs at low nucleation rates where larger errors are acceptable. At higher nucleation rates an almost perfect fit is obtained.



**Figure 3.** Nucleation rate as a function of ammonia mixing ratio at T = 258.15 K and T = 298.15 K. Total sulfuric acid concentration (in molecules cm<sup>-3</sup>) is indicated for each curve. Parametrizations are shown as dotted lines. Relative humidity is 50%.



**Figure 4.** Dependence of nucleation rate on relative humidity at T = 258.15 K and T = 298.15 K. Ammonia mixing ratio (in ppt) is indicated in the figure. Parametrizations are shown as dotted lines.

[18] A common property of Figures 2–4 is that the parametrization is worst at the higher temperature as nucleation rate approaches the lower limit. This reflects the fact that nucleation rate is a strong function of temperature at low nucleation rates, as shown in Figure 5. Also problematic is the inclusion of near-constancy of nucleation rate in the parametrization at low temperatures; nevertheless, the difference between the model and the parametrization is less than about one order of magnitude for all temperatures.



**Figure 5.** Temperature dependence of nucleation rate. Ammonia mixing ratio (in ppt) is indicated for each curve. Relative humidity is 50%. Parametrizations are shown as dotted lines.

[19] Figure 6 shows the number the  $H_2SO_4$  molecules (Figure 6a), number of NH<sub>3</sub> molecules (Figure 6b), total number of molecules (Figure 6c), and the radius of the critical cluster (Figure 6d) as a function of nucleation rate at T = 280 K. The parametrizations from equations (9)–(12) (lines) are compared to model data (dots). The number of  $H_2SO_4$  and  $NH_3$  molecules are almost the same for all the cases considered here. At T = 280 K the total number of molecules in the critical cluster is practically the same as the sum of the H<sub>2</sub>SO<sub>4</sub> and NH<sub>3</sub> molecules, because the number of water molecules is very small (usually less than 1, which can be rounded off to zero). The parametrizations give the particle content with a typical accuracy of one molecule. The difference between the radii from the full nucleation model and the parametrization is about 0.05 nm. The accuracy of the fits (9)-(12) have little dependence on temperature or cluster size.

### 5. Discussion and Conclusions

[20] We have constructed a parametrization of  $H_2O$ -H<sub>2</sub>SO<sub>4</sub>-NH<sub>3</sub> nucleation rates. The parametrization covers gas abundances commonly observed in the troposphere, including upper troposphere. However, the temperature range is somewhat limited at the lower end because the nucleation model is not valid at low temperatures (typically below 240 K). The very highest temperatures (T > 300 K) are omitted because it was impossible to include a wider temperature range in the same fit. Also, we have set the upper limit of ammonia mixing ratio to 100 ppt. This is partly because ammonia mixing ratios greater than 100 ppt do not have much effect on nucleation rate unless  $H_2SO_4$ concentration is very low, partly because a wider range of mixing ratios would make the parametrizations worse. If ammonia mixing ratio exceeds 100 ppt, we recommend using values obtained with 100 ppt.

[21] The parametrization reproduces the nucleation rates obtained from the full model usually within the range of one order of magnitude in general. The fit is worst at high temperatures and low nucleation rates. We do not consider this as a serious problem, because at significant nucleation rates (J > 0.01-0.1 cm<sup>-3</sup> s<sup>-1</sup>) the fit is more accurate and, thus, adequate for atmospherically related purposes.

[22] No matter how good is the parametrization, there still is a question of the validity of nucleation model itself, and ultimately the model should be compared to experiments. Unfortunately, there is no experimental data available for such a comparison. However, we know that classical nucleation model fails close to the binary  $H_2O-H_2SO_4$  limit [*Napari et al.*, 2002]. Therefore, we have excluded the data points with less than 0.1 ppt of ammonia from our parametrizations.

[23] The presented parametrization is the first relevant parametrization for ternary nucleation rates and it can be

**Figure 6.** (opposite) Number of  $H_2SO_4$  molecules (a), number of NH<sub>3</sub> molecules (b), total number of molecules (c) in the critical cluster, and the radius of the critical nucleus (d) as a function of nucleation rate at T = 280 K. Dots describe data from the full model while the lines are parametrizations. The gas concentrations in each plot are within the limits given in the text.



used as a subroutine for different types of aerosol dynamic models. Compared with the full model it saves computing time by a factor of  $10^5$ .

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